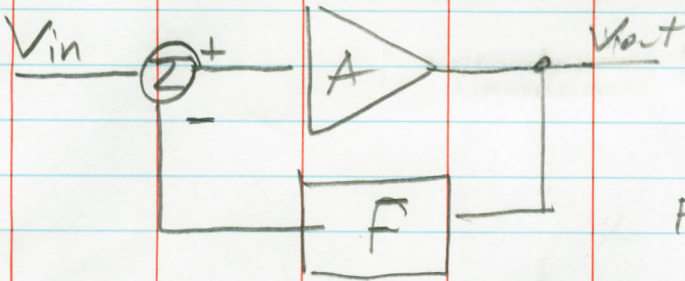


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## Basic Idea of Feedback



$A \equiv$  open loop gain ( $A \gg 1$ )  
 $F \equiv$  Fraction of feedback signal ( $F < 1$ )  
 Typically  $F \ll 1$  and  $A \gg 1$ .

$$A(V_{in} + FV_{out}) = V_{out}$$

$$\therefore \frac{V_{out}}{V_{in}} = \frac{A}{1+AF}$$

$$\text{" } \xrightarrow{A \rightarrow \infty} \frac{1}{F}$$

2 Closed loop gain  $\equiv G = V_{out}/V_{in}$

$$\therefore G = \frac{A}{1+AF}$$

$$\frac{\partial G}{\partial A} = \frac{(1+AF) - AF}{(1+AF)^2} = \frac{1}{(1+AF)^2} = \frac{1}{A}$$

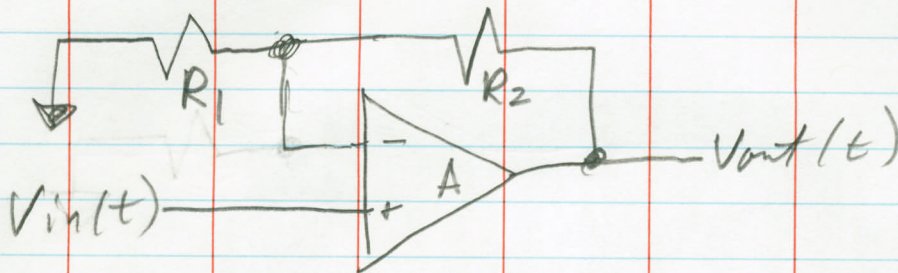
$$\frac{\Delta G}{G} = \frac{A}{(1+AF)^2} \cdot \frac{(1+AF)}{A} \cdot \frac{\Delta A}{A}$$

$$\text{" } = \frac{1}{1+AF} \cdot \frac{\Delta A}{A}$$

decrease sensitivity to variation in A.

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Example of non-inverting voltage amp



$$\textcircled{1} \quad \frac{V_+}{R_1} + \frac{V_- - V_{out}}{R_2} = 0 \quad \Rightarrow \quad V_- = V_{in} - \frac{V_{out}}{A}$$

$$\textcircled{2} \quad A(V_{in} - V_-) = V_{out} \quad \Rightarrow \quad V_- = \frac{R_1}{R_1 + R_2} V_{out}$$

Now, let  $F = \frac{R_1}{R_1 + R_2}$ ; the divider part

$$V_{out} \left( \frac{R_1}{R_1 + R_2} + \frac{1}{A} \right) = V_{in}$$

$$V_{out} \left( F + \frac{1}{A} \right) = V_{in} \quad \text{when } F \equiv \frac{R_1}{R_1 + R_2} \text{ from}$$

$$G \equiv \frac{V_{out}}{V_{in}} = \frac{A}{1 + AF}$$

voltage divider

$$\frac{\Delta G}{G} = \frac{1}{AF + 1} \left( \frac{\Delta A}{A} \right)$$

Suppose  $A = 10^6$ ,  $F = 10^{-2}$  (closed loop gain  $1 + F = 1.01$ )

$$\frac{\Delta G}{G} = (10^{+4}) \frac{\Delta A}{A} !$$

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(3)

Feedback can be used to increase the bandwidth of a system at the expense of gain

$$G = \frac{A}{1+AF} \quad \text{Suppose } A = \frac{A_0 \overset{\text{Gain at } \omega \rightarrow 0}{\leftarrow}}{1+\omega/\omega_0}$$

$$\therefore G = \frac{\frac{A_0}{1+(\omega/\omega_0)}}{1 + \frac{A_0 F}{1+(\omega/\omega_0)}} = \frac{A_0}{A_0 F + 1 + (\omega/\omega_0)}$$

$$= \frac{A_0 / (1 + A_0 F)}{1 + \omega / [\omega_0 (1 + A_0 F)]}$$

New gain as  $\omega \rightarrow 0$  is  $\frac{A_0}{1 + A_0 F}$

just as in "DC" case.

New frequency cut-off is  $\omega_0 (1 + A_0 F) > \omega_0$

Note that "Gain-bandwidth product" stays constant at  $(A_0 \omega_0)$ . This makes op-amps useful even as  $A(\omega)$  decreases with frequency.