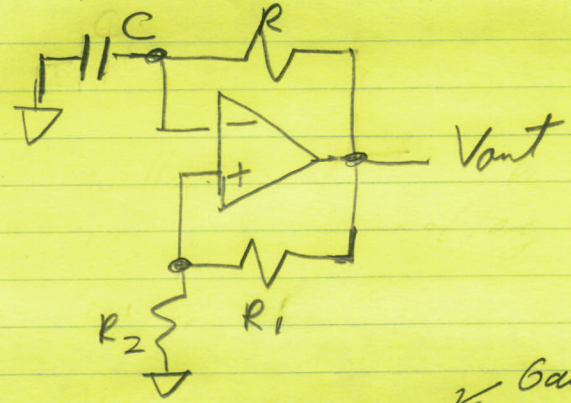


①

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The basic oscillator circuit - Relaxation to a time varying target voltage

Consider the circuit:



Gain, a big number

We know at  $V_{out} = A(V_+ - V_-)$

Since  $V_{out}$  is bounded by  $V_{supply}$ , this means that

$$V_{out} = \begin{cases} +V_{supply} & V_+ > V_- \\ -V_{supply} & V_- < V_+ \end{cases}$$

The voltage divider assures that  $V_-$  is compared to  $V_+ = \frac{R_2}{R_1 + R_2} V_{out}$

$V_-$  will evolve in time according to:

$$C \frac{dV_-}{dt} + \frac{V_- - V_{out}}{R} = 0 \quad ; \quad \tau \equiv RC$$

$$\therefore \frac{dV_-}{dt} + \frac{1}{\tau} V_- = \frac{1}{\tau} V_{out}$$

homogeneous eqn  $\phi(t) = e^{-t/\tau}$

$$V(t) = V(0) e^{-t/\tau} + \int_0^t \left( \frac{1}{\tau} V_{out} \right) e^{-(t-x)/\tau} dx$$

+ treat as constant since last transition

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$$V_-(t) = V(0)e^{-t/\tau} + \frac{1}{\tau} e^{-t/\tau} (\tau) (e^{t/\tau} - 1)$$

$$= V(0)e^{-t/\tau} + V_{out} (1 - e^{-t/\tau})$$

Lets start with  $V(0) = 0$  and pick  $V_{out} = +V_{supply}$ .

$$\text{Then } V_-(t) = +V_{supply} (1 - e^{-t/\tau})$$

$$\text{But when } V_-(t) > V_+ = \frac{R_2}{R_1 + R_2} V_{supply}$$

the value of  $V_{out}$  will change to  $-V_{supply}$ .

This occurs when

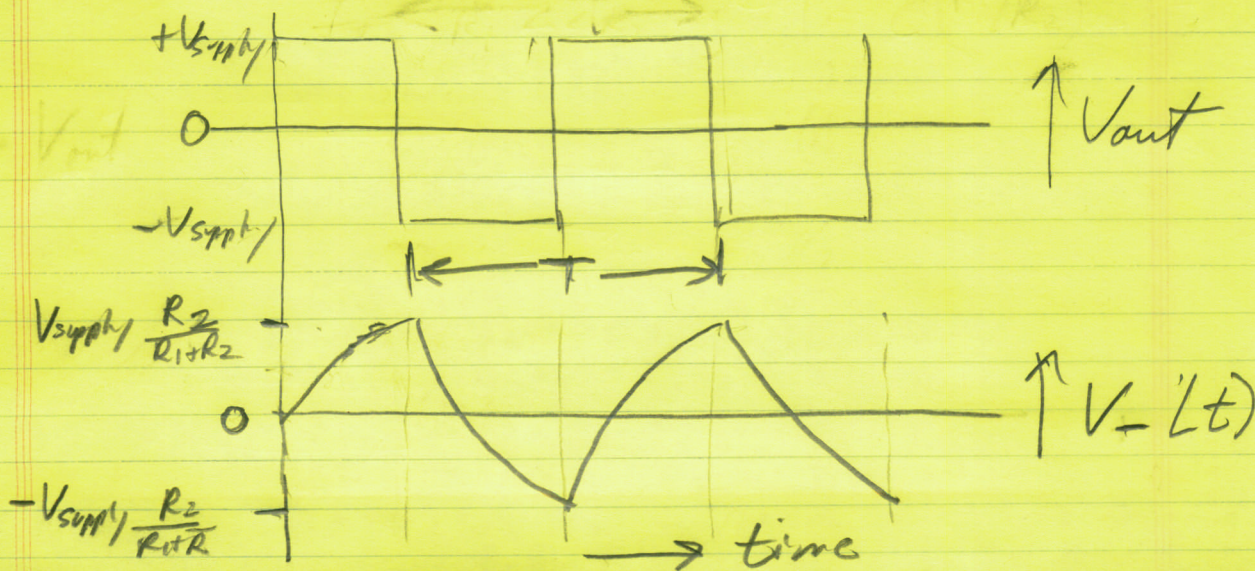
$$V_{supply} (1 - e^{-t/\tau}) = \frac{R_2}{R_1 + R_2} V_{supply}$$

$$e^{-t/\tau} = 1 - \frac{R_2}{R_1 + R_2} = \frac{R_1}{R_1 + R_2}$$

$$t = \tau \log(1 + R_2/R_1) \quad \left( \begin{array}{l} \text{and } R_2 \rightarrow \infty \\ \text{gives } t \rightarrow \infty \end{array} \right)$$

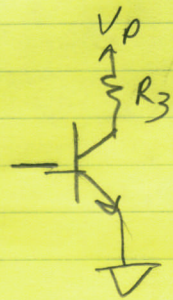
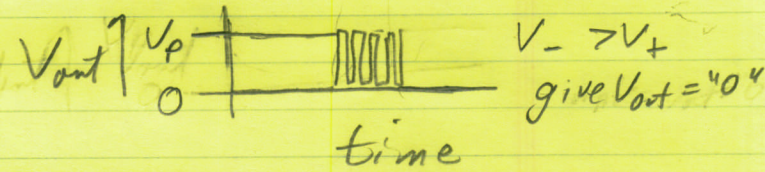
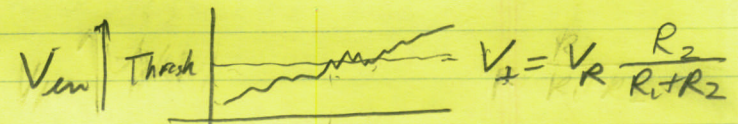
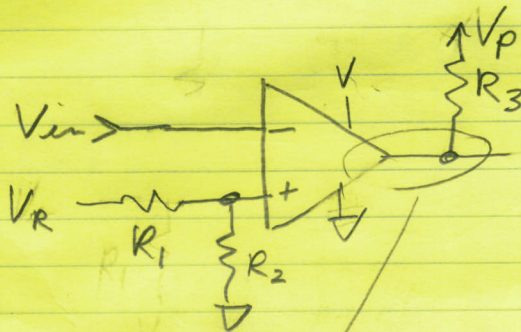
The period is 4 times this, so.

$$T = \tau \log(1 + R_2/R_1)$$

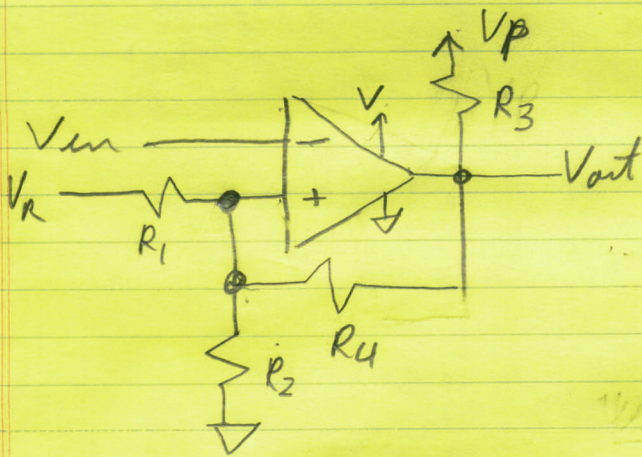


### Schmitt Trigger Notes

This is a "tip" to minimize hysteresis with comparator.



Pullup resistor  $R_3$  is used in most comparators as output is an "open collector", so that user can define output voltage.



Pick  $V_p$  to equal  $V_R \frac{R_2}{R_1 + R_2}$

$$V_{out} = \begin{cases} 0 & V_{in} > V_+ \\ V_p & V_{in} < V_+ \end{cases}$$

and KVL gives

$$\frac{V_+ - V_R}{R_1} + \frac{V_+}{R_2} + \frac{V_+ - V_{out}}{R_4} = 0$$

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Case of  $V_{out} = 0$

$$V_+ \left( \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_4} \right) = \frac{V_R}{R_1}$$

$$V_+ \left( \frac{R_1 + R_2}{R_1 R_2} \right) \left[ 1 + \frac{R_1 R_2}{R_1 + R_2} \frac{1}{R_4} \right] = \frac{V_R}{R_1}$$

$$V_+ = V_R \frac{R_2}{R_1 + R_2} \left[ \frac{1}{1 + \frac{R_1 R_2}{R_1 + R_2} \left( \frac{1}{R_4} \right)} \right] V_R$$

denominator  $> 1$ , so  $[ ] < 1$

$$\therefore V_+ < \frac{R_2}{R_1 + R_2} V_R$$

reduced threshold when output is "0"

Case of  $V_{out} = V_P$

(Assume to be  $V_P$ )

$$V_+ \left( \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_4} \right) = \frac{V_R}{R_1} + \frac{V_P}{R_4}$$

$$V_+ = \frac{R_1 R_2}{R_1 + R_2} \left[ \frac{1}{1 + \frac{R_1 R_2}{R_1 + R_2} \frac{1}{R_4}} \right] \left( \frac{V_R}{R_1} + \frac{V_P}{R_4} \right)$$

$< 1$

$$V_+ = V_R \frac{R_2}{R_1 + R_2} \left[ \frac{1}{1 + \frac{R_1 R_2}{R_1 + R_2} \frac{1}{R_4}} \right] \left[ 1 + \frac{R_1}{R_4} \frac{V_P}{V_R} \right]$$

$< 1$

$> 1$

$\therefore$  We can have

$$V_+ \geq \frac{R_2}{R_1 + R_2} V_R$$

Simple case is  $R_1 = R_2$ ;  $R_4 = 10R_1$ ;  $V_R = 2V_P$ .

$$\left[ \frac{6V_R}{1 + \frac{R_1}{R_2}} \right]$$

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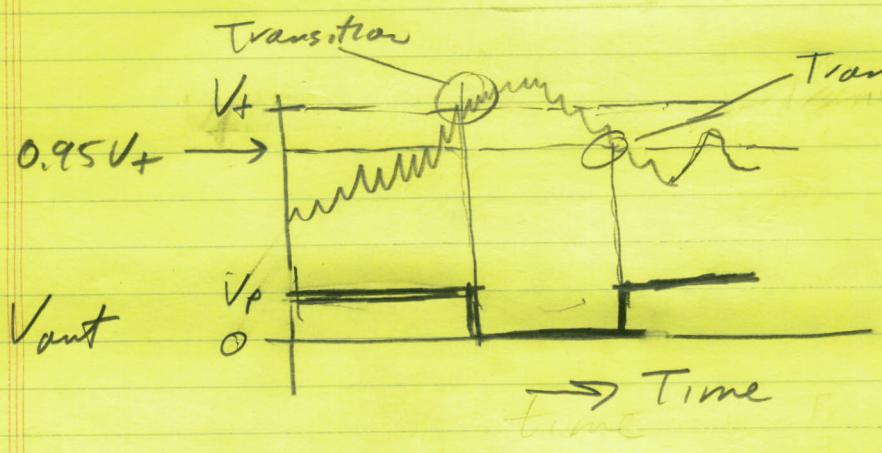
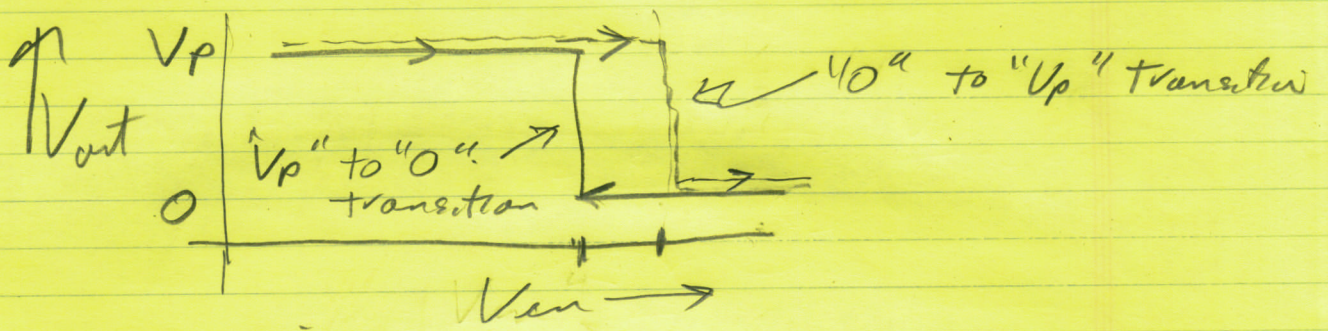
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$$\left[ \frac{1}{1 + \frac{R_1 R_2}{R_1 + R_2} \frac{1}{R_4}} \right] = \dots = \frac{1}{1.05}$$

$$\left[ 1 + \frac{R_1}{R_4} \frac{V_p}{V_R} \right] = \dots = 1.05$$

∴ The threshold voltage is

$$V_t = \begin{cases} \frac{V_p}{2} \cdot \frac{1}{1.05} = \frac{V_p}{2} (0.95) ; V_{out}(t=0^-) = 0 \\ \frac{V_p}{2} \cdot \frac{1}{1.05} \times 1.05 = \frac{V_p}{2} ; V_{out}(t=0^-) = V_p \end{cases}$$

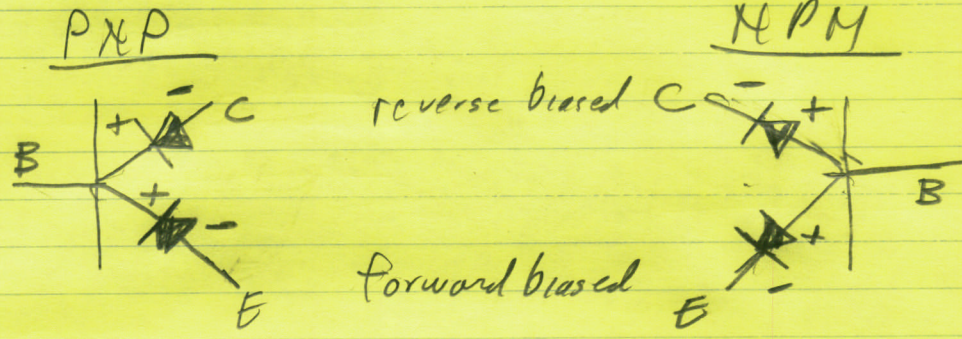
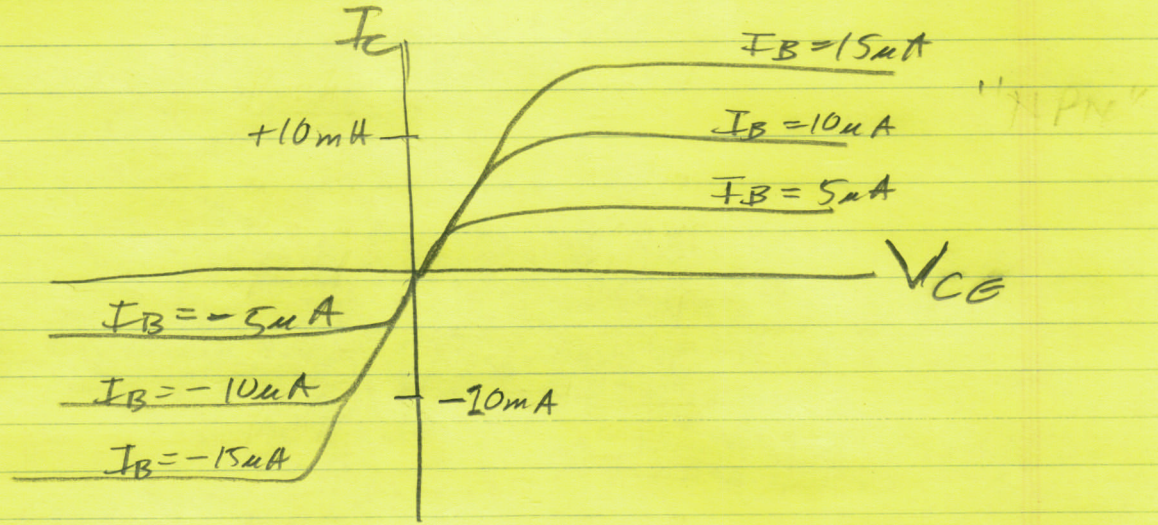


Again, recall that for  $V_{in} = V_{in} > V_t$  the output is "0"

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Notes on "push-pull" circuit. (8.8)

This is a circuit with two emitter followers, one that uses a NPN transistor for  $I_B > 0$  and one that uses a PNP transistor for  $I_B < 0$ .



The "push-pull" circuit allows you to source a large current to the load.