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# Modal Analysis of Percussion Instrum

## Using Vibrational Holography

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### • Abstract

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- Many musical instruments, including numerous percussion instruments, produce sound from vibrating plates. With vibrational holography, we gain very accurate information about the patterns of vibration (modal patterns). Time-average vibrational holography uses two beams of a coherent laser on a high-resolution holography film. One beam is a fixed path length reference beam, while the object beam is incident on the vibrating plate. As the vibrating plate changes the path length of the object beam, it creates interference fringes about the antinodes of vibration. We studied systems of increasing complexity, starting with a simple case of a uniform circular plate. We then considered various metal plates, such as specialty cymbals, and hand bells. In real-time vibrational holography, it is necessary to produce a plate hologram of the vibrating plate. We develop the plate and place it back in the holder, superimposing the real object. If we vibrate the object, there will be interference between the image of the hologram and the vibrating object. We use a beam splitter to slow down the interference shifts throughout the period of the vibration. This technique is used to study modal patterns in a cymbal.

### • Introduction

All sound can be thought of as a superposition of pure sine waves. We can represent this as a displacement versus time on a graph which, because of simple harmonic motion, will result in a sine wave. When an object vibrates at multiple frequencies, its representative wave becomes no longer a simple sine wave, but a complex wave, not easily describable with simple trigonometry. We know that this wave can be broken up into several sine waves with distinct frequencies using Fourier transformation. If an object vibrates at those distinct frequencies, known as resonance or modes, we can predict what sound it will create.

Ernst Chladni was the first to study these modes in 1787. He used flat plates, now known as Chladni plates, to study the vibrational behavior of flat surfaces. The classic plate is of a uniform thickness and shape. Understanding of the natural modes of vibration. It is difficult to analyze modes of vibration with the naked eye, the plate does not appear to move. To study this, we need to drive the plate at its natural frequencies. Chladni did this by bowing the plates, and we are able to do it with a small-mass driving magnet and electromagnetic drive coil. Certain modes, dependent on the metal, the shape, and the thickness, will resonate with specific frequencies. A circular plate will vibrate with nodal diameters and nodal circles. An elementary way to study this is to use sand and drive the plate at its resonant frequencies. The sand will move to the lines on the plate, called nodal lines. The result is a plate with sand lines at the nodes of vibration, which gives us a good idea of the manner of vibration. This technique relies on the assumption that the sand is massless and moves with little force at all. It is also limited by the fact that the surface mu

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horizontal and relatively flat. Unfortunately this is rarely the case.

A much more sensitive and versatile way to understand the production of sound is by using holography. The technique of vibrational holography applies what we know of optics and to study the vibrational modes of vibrating surfaces. Vibrational holography, or holography, uses laser superposition to either constructively or destructively interfere a reference and object where the previously mentioned nodal or antinodal areas of the plate vibrate.

As with any study using wave superposition, it is necessary to have a single coherent wave interference. Please refer to Figure 1. One He-Ne laser is used and split into two beams with a reflective mirror. One beam, the object beam, travels along a path to the object. The object is given frequency by a contact magnet. The laser is reflected off of the object to an emulsified glass plate. The other beam, the reference beam, follows a different path. On the emulsion of the holographic plates, there will be an interference pattern on the plate that is dependent on the different path lengths.

If our object is not vibrating, there will be interference at many different levels due to the path differences. The interference from the path differences creates a complex diffraction pattern. As we develop our plate, the areas of constructive interference become spots on the film. When we view the image, we will diffract the reference beam to form a virtual image of our object from the complex diffraction pattern.

When an object is vibrating in a sinusoidal manner, it spends most of its time at the point of zero displacement. The interference pattern created when the vibrating object is at the positive maximum displacement will emphasize certain areas in the grid of the points of interference. As we create our visualization of the vibration, while the plate is in between the positive and negative maximum displacement, the result on our plate is *averaged out* in the time average and, therefore, does not embellish the object. As the object vibrates, the path length will be changed from positive amplitude to negative amplitude. On the emulsified glass plate, the two wave fronts interfere depending on how much that particular vibrating surface moved. Because the laser wavelength is on the order of 632.8 nm (6.328 x 10<sup>-7</sup> m), the surface must only move about one half of a wavelength to change from constructive interference to destructive interference. Because of the small wavelength produced by the laser, spatial resolution is high. These fringes get closer together when the path difference increases and a bullseye pattern is created where the antinodes are located, surrounded by a nodal circle. We can study these functions to help us describe the vibration of the object.

### • Theory

As an introduction, we can look at the behavior of a single exposure hologram, reconstructing the field of the following:

We can show the  $E$  field incident on a holographic plate is simply the function of a vector field (the reference beam and the object beam).

$$E_{ref} = r e^{i\omega t} e^{i \frac{2\pi}{\lambda} x \sin(\alpha)}$$

$$E_{obj} = s e^{i\omega t} e^{i \frac{2\pi}{\lambda} x \sin(\beta)}$$

As in most cases, what is recorded is the irradiance of the total field. We can show:

$$I = (E_{\text{subj}} + E_{\text{ref}})(E_{\text{subj}}^* + E_{\text{ref}}^*)$$

$$I = r^2 + s^2 + E_{\text{subj}} E_{\text{ref}}^* e^{i(2\pi \frac{2\pi \sin(\alpha)}{\lambda} x)} + E_{\text{ref}} E_{\text{subj}}^* e^{-i(2\pi \frac{2\pi \sin(\beta)}{\lambda} x)}$$

This irradiance is recorded on the film as a light and dark pattern (a diffraction pattern if you reilluminate the film with the reference beam, the transmitted electric field will have an envelope attenuated (albeit nonuniformly) by the pattern on the film.

Now we can show through a series of calculations, that the resultant electric field created when we reilluminate the holography plate with just the reference beam:

$$E_{\text{reilluminated}} = (r^2 + s^2) E_{\text{ref}} + r^2 s e^{i(\alpha x + \frac{2\pi}{\lambda} x \sin(\alpha))} + r^2 s e^{-i(\frac{2\pi}{\lambda} x \sin(\beta))}$$

The first term of this is actually the reference beam, modulated in amplitude but not phase. The incident beam passes through the film unchanged. The second term describes the electric field that comes from the object. The third term actually is the  $E$  field due to a *real image* of the subject, important to our data.

The phase of this second term is due to the term  $x \sin(\alpha)$ . This phase is for only a single point. If we look at a moving source, we must take into consideration the optical path length difference. This can be explained with respect to the unit vector  $n_1$ , representing the direction of illumination,  $n_2$  the direction of recording (or the direction to the film), and  $n_m$ , the direction of vibration.

$$\Delta = A n_m \cdot (n_1 + n_2)$$

$A$  is the displacement of vibration at any particular point on our object. If we change this by multiplying it by  $\sin(\alpha t)$ , we get an  $E$  field as follows:

$$E = E_0 e^{i(\frac{2\pi}{\lambda} A n_m \sin(\alpha t))}$$

where  $E_0$  is a function varying with time as:

$$E_0 = r^2 s e$$

If we take the time average of this function, we get the integral:

$$\langle E_{\text{irradiance}} \rangle = E_0 \frac{1}{T} \int_0^T e^{i(\frac{2\pi}{\lambda} A n_m \sin(\alpha t))} dt$$

According to Brown, Grant, and Stroke, this image has an intensity that goes like a first or

$$I = |E_0|^2 \left| J_0 \left( \frac{2\pi}{\lambda} Am_m \cdot (n_1 + n_2) \right) \right|^2$$

This equation is the intensity of a single point on our object, but can be used to describe an object with some creative thinking. If we think of every point on our object as a single sum over all points to reconstruct the object.

This technique of time-average holography has been used at length studying the production instruments such as classical and acoustic guitar, percussion instruments such as snare drum and steel drums.

Vibrational interferometry research at Stetson University was initiated in 1996 with Frank research under Dr. Kevin Rigg's mentoring on *Modal Analysis of Musical Instruments Using Holography*. Stetson now has an active acoustical holography lab that is ready for in depth summer of 1996 the lab was used to analyze the modes of steel drums and guitar bodies. It for research on a subject that has not previously been investigated anywhere.

In this case (1997), we will be examining the complex plates found in Turkish and Chinese. These specimens, specifics to be named later, have the more complex variable thickness and center bells. These will produce more complex modes of vibration, changing and bend of the cymbal. The Turkish cymbal, for example, tends to be of a thicker brass, which means amplitude of the vibrations will be less. In comparison, the Chinese cymbals have more of the edge of the cymbal the plate folds up at an angle.

There is also a technique using these interference patterns called *real-time interferometry*. exposure of the object that is not vibrating and develop the plate, we can replace it in the gravity plate holder using ball bearings and set-pins. This plate holder restricts all six degrees that we can superpose the hologram and the object. When we set the Chladni plate in vibration pattern appears on the object and, therefore, is called *live-fringe*. We will be using the lab nondestructive testing also. We will use video and photography to record this.

We will be using photography and emulsified glass plates as a record medium for our find Chladni plates, and define each of the resonating frequencies into the accepted form of (m diameters, and n= nodal circles. There are bound to be some perturbations from the classic to the complex nature of the system. Though this is too complex to solve directly, we can physics and solve it numerically.

- *G<sub>3</sub> Hand Bell-Amplitude Analysis*

We can learn about the amplitude analysis ability of vibrational holography. We can look the hand bell at two different amplitudes (Fig 1 -2):

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Figure 1-(3,1) mode being driven at -80.2 dB (relative)

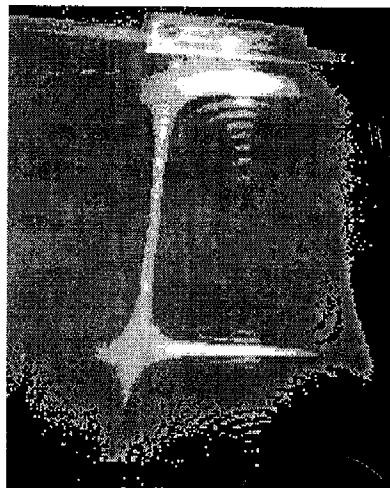


Figure 2-(3,1) mode driven at -50.0 dB (relative)

If you notice, the nodal lines and circles are in the same places, letting us know it is the same confirmed by looking at the holography log and noting that they were both done when driven at 1342.3 Hz. The driving amplitudes are measured with a near-field microphone in decibels. The dB scale is a logarithmic scale. We can describe the *Sound Intensity Level* ( $SIL$ ) defined as:

$$SIL = 10 \text{Log} \left( \frac{I}{I_0} \right)$$

where  $I$  is intensity, which is proportional to displacement squared.

If we look at comparing two levels, we can show:

$$SIL_1 = 10 \text{Log} \left( \frac{I_1}{I_0} \right)$$

$$SIL_2 = 10 \text{Log} \left( \frac{I_2}{I_0} \right)$$

$$SIL_2 - SIL_1 = 10 \text{Log} \left( \frac{I_2}{I_0} \right) - 10 \text{Log} \left( \frac{I_1}{I_0} \right) = 10 \left[ \text{Log} \left( \frac{\frac{I_2}{I_0}}{\frac{I_1}{I_0}} \right) \right] = 10 \text{Log} \left( \frac{I_2}{I_1} \right)$$

$$SIL_2 - SIL_1 = 10 \text{Log} \left( \left( \frac{d_2}{d_1} \right)^2 \right) = 20 \text{Log} \left( \frac{d_2}{d_1} \right)$$

If we look at our specific case, we can calculate the ratio of  $d_2/d_1$  is 3.16. If we assume the function of interference, we should be able to count up the number of fringes and take the Fig.15/Fig.14. When we do this, we get 3, which compares very well. The difference is due to assumption of linear functionality, and the fact that when we count the fringes, this is a quantity which would not give us a fraction as a ratio. Actually the fringes correspond to zeros of  $B$ . Our calculation is rough approximation is hopeful for a future paper that studies more accurately the dependency of vibrational holograms.

## • Conclusion

There are many applications for this technique in industry. The method of vibrational holography can be used to study stress in turbines among other things. In our particular laboratory, we specialize in percussion instruments, particularly of the cymbal family. These metal subjects are divided into two families: those that are clamped at the edges, and those free to vibrate. The cymbals were the ones that were free to vibrate at the edges. These were successfully modeled by a uniform circular plate. Even a hand bell could conform to this model. The thickness, and contour of the actual cymbal were relatively negligible, until we studied the Mini-Chinese® Cymbal, and the Paiste Alpha Splash® Cymbal where the non-uniformity of the cymbal were too great to conform to the uniform plate model. They should have been modeled by the square plate clamped at the edges, the modes of which would have been different. This was no doubt due to the fact that the notes on a steel drum are not square, but if we made a regular shape, it would be that of a trapezoid. The thickness variations due to the hammering also play an important role in the normal modes of vibration.

There were several problems with the execution of this technique that need to be dealt with. The first is the topic of coherence length. Unfortunately, the He-Ne laser used in this experiment had a coherence length that was only 20-30 cm. The attention paid to the coherence length and its relation to the path length difference however should have been greater. This lack of attention leads to a contrast in the holograms that was less than that achievable. In the future, there should be more of a greater amount of time spent on the contrast in the holograms but matching the path lengths. This lack of contrast led to the poor results from this paper.

The second of our problems had to do with the issue of photographing our holograms. We placed the film close to our subject so that we could collect as much light reflected off the vibrating surface as possible. We were still able to evaluate each subject's modal attributes despite the parallax phenomena available in the hologram. Unfortunately however, the camera due to the parallax of the hologram, and therefore in some of the subjects, our publishable data (photographs) turned out to be simply unpublishable. We need to take this into consideration for future work.

In the vein of the photographs, one of the most difficult things in post-research processing is the quality of the photographs of the holograms. Though the best results quickly came from high speed photography (i.e. exposure times of  $3.125 \times 10^{-4}$  s), the nature of this film is that there are large crystals of silver halide in the film to collect as much light as possible. The high resolution achieved by the holographic process is drastically reduced in this process. Theoretically, we should be able to use much slower film for high resolution photography is also done in a light vacuum room, similarly to the exposure of the hologram. It would be too difficult to spend a little more time at perfecting this portion of the research to attain publishable data.

Some of the records or subject modes were damaged in developing the actual holography. We must remember that the emulsion is not fixed to the plastic (or glass) backing. In developing the hologram, we must remember this fact and not damage the emulsification of the holography film.

As a whole, we were able to successfully perform modal analysis on our subjects. We would have liked to have prevented us from using this highly sensitive method of vibrational study. The preliminary "rough" fit of amplitude analysis, a future endeavor is logically to study the amplitude analysis on our subjects. The work involved is simply to further research of the equation involving Bessel functions

$$I = |E_0|^2 \left| J_0 \left( \frac{2\pi}{\lambda} A m_{mn} (n_1 + n_2) \right) \right|^2$$

The amplitude information falls out of this equation. The data is taken and there is no lab necessary for this, though better contrast holograms and better photographs would be recorded.

Future projects from this are numerous. In the summer of 1998, research is planned for ins of TV holography, a method of real time Interferometry *directly* incident on a camera lens wave-recombiner. TV Holography is a much more efficient and will prove to be very usef

